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Mode III interfacial crack in the presence of couple-stress elastic materials

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Abstract

In this paper we are concerned with the problem of a crack lying at the interface between dissimilar materials with microstructure undergoing antiplane deformations. The micropolar behaviour of the materials is described by the theory of couple-stress elasticity developed by Koiter (1964). This constitutive model includes the characteristic lengths in bending and torsion and thus it is able to account for the underlying microstructure of the two materials. We perform an asymptotic analysis to investigate the behaviour of the solution near the crack tip. It turns out that the stress singularity at the crack tip is strongly influenced by the microstructural parameters and it may or may not show oscillatory behaviour depending on the ratio between the characteristic lengths.

Keywords:

Interface fracture; Couple stress elasticity; Asymptotic analysis; Stress singularity

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Nomenclature

G_{\pm}	shear modulus (+/- stands for upper/lower half-plane)
ν_{\pm}	Poisson's ratio
l_b^{\pm}	material characteristic length in bending
l_t^{\pm}	material characteristic length in torsion
l_{\pm}	material characteristic length (Koiter's notation)
η_{\pm}	ratio between the characteristic lengths in bending and torsion (Koiter's notation, $-1 < \eta_{\pm} \leq 1$)
\mathbf{u}	displacement field
w	out-of-plane displacement
φ	rotation vector
ϵ	strain tensor
χ	curvature tensor
\mathbf{t}	nonsymmetric stress tensor
σ	symmetric part of the stress tensor
τ	skew-symmetric part of the stress tensor
μ	couple-stress tensor
\mathbf{p}	reduced tractions vector
\mathbf{q}	reduced couple-stress tractions vector
λ	order of stress singularity

1 Introduction

Nowadays, bimetals are efficiently and widely used in many advanced engineering applications, such as layered composite structures, electronic packaging and thin film coatings. For the prediction of failure of these structures and the assessment of acceptable stress level under the condition experienced during service, it becomes essential to estimate the magnitude and distribution of the interfacial stress and strain fields along the interface and mainly near the tip of interface cracks, which may arise and extend under general loading conditions. In particular, antiplane shear loading condition may frequently occur in the life span of composite structures, both alone or accompanied by plane deformation.

Within the classical LEFM theory, the crack tip fields for an interface crack under antiplane strain are similar to the Mode III crack tip fields in a homogeneous medium (Willis, 1971; Piccolroaz et al., 2009). In both cases, indeed, the shear stresses on the crack plane are the same in the upper and lower bodies, whereas the out-of-plane displacement is zero on the uncracked region of the crack plane. Thus, it is possible to combine the lower and the upper bodies to obtain equilibrium, without changing displacements or stresses in the two halves. Stresses exhibit Mode III symmetry, but displacements do not and thus crack sliding profiles are not symmetric.

Due to the lack of a length scale, the classical theory of elasticity is not able to characterize the constitutive behaviour of brittle materials at the micron scale. This lack is expected to be particularly significant for the analysis of the stress and deformation fields very near the crack tip. For a proper investigation of the crack tip fields at the micron scale it becomes necessary to adopt enhanced constitutive models, which account for the presence of microstructure. A way of doing that consists in the inclusion of one or more characteristic lengths, typically of the same order of the compositional grain size, generally few microns, for many advanced materials. The indeterminate theory of couple-stress elasticity (CSE) developed by Koiter (1964) involves the material characteristic lengths in bending and torsion. It is sufficiently accurate to simulate the behaviour of materials at the micron scale as well as the size effects occurring at distances to the crack tip comparable to characteristic lengths, but it is also simple enough to allow the achievement of closed-form solutions.

Although the presence of the microstructure is expected to modify the interface crack tip field with respect to the classical solution of the LEFM, no analytical investigations have been so far performed about the problem of an antiplane crack along the interface between micropolar and classical elastic materials (the only related work regards a crack terminating perpendicular to the interface; Mishuris, 1985). Most of related studies available in literature instead concern the problem of an interface crack under plane deformations, e.g., Itou (1991) examined the effect of couple-stresses on the strain energy release rate for an interface crack loaded by an internal pressure, neglecting somehow the oscillatory behaviour of the crack tip fields.

In order to provide an experimental basis for studying the interfacial behaviour of a bimaterial specimen under shear loading, Kang et al. (2002) applied a method which combines moiré interferometry with phase shift and image processing to measuring the interfacial displacement and strain fields within the interfacial region. Their experimental results show that there is a boundary layer characteristic with a peak value of shear strain and high gradient of rotation angle in the interfacial region. Their study also shows that similar results can be analytically predicted by means of the couple-stress theory, considering the additional freedom of the rotation angle effect.

Hutapea et al. (2003) investigated the micro-stress generated along a fiber/matrix interface under generalized plane deformation, which are expected to dominate the failure initiation process in composite laminate. They showed that the micropolar theory is able to capture the interface micro-stress accurately.

A small number of interface crack problems have been investigated by using the strain gradient theory of plasticity (Hao and Liu, 1999; Chen and Wang, 2002). In particular, Hao and Liu (1999) analyzed the crack propagation in bimaterial systems showing that high stress triaxiality always occurs on the softer material, which may promote ductile damage and facilitate crack growth. Chen and Wang (2002) explored the interface crack tip fields at micron scales under plane strain conditions. Their numerical

investigations show that the singularity of stresses in the strain gradient theory slightly exceeds or equals to the square-root singularity independently of the material hardening exponents. Askes and Gitman (2009) showed numerically that in gradient elasticity no singular behaviour is found for a crack terminating perpendicular to the interface.

The analysis of singular stress concentration in homogeneous micropolar elastic solids shows that several pathological predictions of classical elasticity in singular stress concentration problems are altered, mitigated, or possibly eliminated when couple-stresses are taken into account (Nazarov and Semenov, 1980). In particular, the problem of a Mode III crack in a homogeneous materials modelled by the couple-stress elastic theory was first analyzed by Zhang et al. (1998) and later by Geogiadis (2003) by considering a single characteristic length. The results obtained therein indicate that the skew-symmetric stress components have $r^{-3/2}$ singularity near the crack tip, where r is the distance to the crack tip. Although this singularity is much stronger than the conventional square-root singularity, it does not violate the boundness of strain energy surrounding the crack tip and leads to a finite energy release rate. Their asymptotic analysis also provides a negative out-of-plane displacement ahead of the crack tip. This unphysical result is due to the exclusion of the lowest order terms for the displacement and symmetric stress components, which do not contribute to the energy release rate.

The effects of both characteristic lengths in bending and torsion and a complete investigation of the crack tip fields under Mode III loading condition in homogeneous CSE materials have been properly addressed in a recent work by Radi (2008). The roles of both characteristic lengths are therein examined in detail and their influence on the crack tip is analytically explored by using Fourier transform and the Wiener-Hopf method. The asymptotic and full-field analyses show that the symmetric stress is finite at the crack tip, whereas the skew-symmetric stress is negative and strongly singular. Ahead of the crack tip within a zone smaller than the characteristic length in torsion, both the total shear stress and reduced tractions occur with the opposite sign with respect to the classical LEFM solution, as predicted by the asymptotic analysis. However, the zone of dominance of the asymptotic fields has limited physical relevance and becomes vanishing small for a characteristic length in torsion of zero. In this limit, the full-field solution recovers the classical K_{III} field with square-root stress singularity. Outside this zone, the total shear stress exhibits a positive maximum, thus providing more realistic predictions on the tractions level ahead of the crack tip than the singular LEFM solution. A sharp crack profile is also observed. It may denote that the crack becomes stiffer, thus revealing that the presence of microstructures may shield the crack tip from fracture.

In the present work, the effects of strain rotation gradients on a stationary antiplane crack along the interface between two different couple-stress elastic materials are analytically investigated by performing an asymptotic analysis of the crack-tip fields. The special problem of a crack along the interface between a couple-stress elastic solid and a classical elastic medium is also addressed in Sec. 3. The results of the present asymptotic analysis are expected to hold in a small zone near to the crack tip, whose extent may vary with the size of the characteristic lengths, and provide valuable information for performing a full-field analysis of the interface crack problem, e.g., by using the Wiener-Hopf method, which will be the subject of further investigations.

2 Crack at the interface between couple-stress elastic materials

We consider a bimaterial plane made of two dissimilar materials, joined along a perfect interface. The two materials are assumed to have an underlying microstructure, described by the material characteristic lengths in bending and in torsion, denoted by l_b^\pm and l_t^\pm , respectively. The elastic moduli are denoted by G_\pm (shear modulus) and ν_\pm (Poisson's ratio). A semi-infinite plane crack is placed along the interface, and a Cartesian reference system is assumed centred at the crack tip, see Fig. 1.

The fundamentals of the Couple Stress (CS) elasticity theory (Koiter, 1964) can be found in several text books and research papers (see for example Nowacki, 1985; Asaro and Lubarda, 2006; Radi, 2008). It

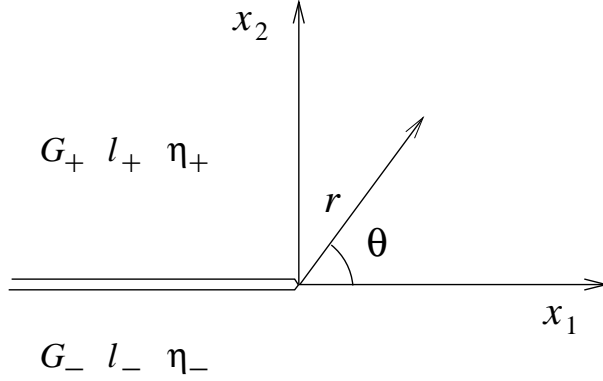


Figure 1: A crack at the interface between dissimilar couple-stress materials.

is recalled here that the main characteristic of this theory is that the rotation vector $\boldsymbol{\varphi}$ is not independent of the displacement vector \boldsymbol{u} , but it is subject to the condition

$$\boldsymbol{\varphi} = \frac{1}{2} \text{curl } \boldsymbol{u}. \quad (1)$$

Consequently, all the kinematical quantities can be derived from the displacement field. In particular, for antiplane shear deformations, the following kinematical relations between the out-of-plane displacement w , rotation vector $\boldsymbol{\varphi}$, strain tensor $\boldsymbol{\varepsilon}$ and curvature tensor $\boldsymbol{\chi}$ are derived

$$\begin{aligned} \varphi_1 &= \frac{1}{2} \frac{\partial w}{\partial x_2}, & \varphi_2 &= -\frac{1}{2} \frac{\partial w}{\partial x_1}, & \varepsilon_{13} &= \frac{1}{2} \frac{\partial w}{\partial x_1}, & \varepsilon_{23} &= \frac{1}{2} \frac{\partial w}{\partial x_2}, \\ \chi_{11} = -\chi_{22} &= \frac{1}{2} \frac{\partial^2 w}{\partial x_1 \partial x_2}, & \chi_{21} &= -\frac{1}{2} \frac{\partial^2 w}{\partial x_1^2}, & \chi_{12} &= \frac{1}{2} \frac{\partial^2 w}{\partial x_2^2}. \end{aligned} \quad (2)$$

An infinitesimal surface element transmits a force and a couple vector, which give rise to a nonsymmetric stress tensor, \boldsymbol{t} , and a couple-stress tensor, $\boldsymbol{\mu}$. The nonsymmetric stress tensor can be decomposed into a symmetric part $\boldsymbol{\sigma}$ and a skew-symmetric part $\boldsymbol{\tau}$, such that $\boldsymbol{t} = \boldsymbol{\sigma} + \boldsymbol{\tau}$.

The isotropic constitutive equations are given by

$$\boldsymbol{\sigma} = \frac{2\nu G(\text{tr } \boldsymbol{\varepsilon})}{1-2\nu} \boldsymbol{I} + 2G\boldsymbol{\varepsilon}, \quad \boldsymbol{\mu} = 2Gl^2(\boldsymbol{\chi}^T + \eta\boldsymbol{\chi}), \quad (3)$$

where \boldsymbol{I} is the identity tensor, l and η the CS parameters introduced by Koiter (1964), with $-1 < \eta \leq 1$, the superscript T denotes transposition. The material parameters l and η characterize the microstructure of the material and can be expressed in terms of the material characteristic lengths in bending and in torsion as follows:

$$l_b = l/\sqrt{2}, \quad l_t = l\sqrt{1+\eta}. \quad (4)$$

For antiplane shear deformations, the nonzero stress and couple-stress components are

$$\sigma_{13} = G \frac{\partial w}{\partial x_1}, \quad \sigma_{23} = G \frac{\partial w}{\partial x_2}, \quad (5)$$

$$\mu_{11} = -\mu_{22} = Gl^2(1+\eta) \frac{\partial^2 w}{\partial x_1 \partial x_2}, \quad \mu_{12} = Gl^2 \left(\eta \frac{\partial^2 w}{\partial x_2^2} - \frac{\partial^2 w}{\partial x_1^2} \right), \quad \mu_{21} = Gl^2 \left(\frac{\partial^2 w}{\partial x_2^2} - \eta \frac{\partial^2 w}{\partial x_1^2} \right). \quad (6)$$

In the absence of body forces and body couples, the equations of equilibrium read

$$\operatorname{div} \mathbf{t}^T = 0, \quad \operatorname{div} \boldsymbol{\mu}^T + (\boldsymbol{\tau} \mathbf{e}_1) \times \mathbf{e}_1 + (\boldsymbol{\tau} \mathbf{e}_2) \times \mathbf{e}_2 + (\boldsymbol{\tau} \mathbf{e}_3) \times \mathbf{e}_3 = 0, \quad (7)$$

where $\{\mathbf{e}_1, \mathbf{e}_2, \mathbf{e}_3\}$ is an orthonormal basis. For antiplane shear deformations, the nonzero skew-symmetric stress components, derived from (6) and (7)₂, are

$$\tau_{13} = -\frac{Gl^2}{2} \Delta \frac{\partial w}{\partial x_1}, \quad \tau_{23} = -\frac{Gl^2}{2} \Delta \frac{\partial w}{\partial x_2}, \quad (8)$$

where Δ stands for the laplacian operator.

In the CS theory, due to the internal constraint (1) between rotations and displacements, the Neumann boundary conditions are prescribed in terms of the so called reduced force tractions vector \mathbf{p} and couple tractions vector \mathbf{q} defined as

$$\mathbf{p} = \mathbf{t}^T \mathbf{n} + \frac{1}{2} \nabla \mu_{nn} \times \mathbf{n}, \quad \mathbf{q} = \boldsymbol{\mu}^T \mathbf{n} - \mu_{nn} \mathbf{n}, \quad (9)$$

respectively, where \mathbf{n} denotes the outward unit normal and $\mu_{nn} = \mathbf{n} \cdot \boldsymbol{\mu} \mathbf{n}$. Additionally, if the external surface of the body is not smooth but piecewise smooth, the boundary conditions include the following equation along each edge

$$Q = \frac{1}{2} (\mu_{nn}^+ - \mu_{nn}^-), \quad (10)$$

where Q is a prescribed line load tangential to the edge (Koiter, 1964), and superscripts $+$ and $-$ stand for the values on the surface at each side of the edge. It then appears that the condition (10) becomes essential in the case of bodies with non-regular boundaries, such as cusps, wedges and cracks.

A substitution of (5) and (8) into (7)₁ gives the following governing equation for the displacements w^\pm in the two half-planes:

$$\Delta w^\pm - \frac{l_\pm^2}{2} \Delta^2 w^\pm = 0, \quad (11)$$

where Δ^2 denotes the bilaplacian operator.

We assume that the crack faces are traction-free, so that the following boundary conditions apply for $x_2 = 0^\pm$ and $x_1 < 0$:

$$\begin{aligned} p_3^\pm &:= G_\pm \left\{ \frac{\partial w^\pm}{\partial x_2} - \frac{l_\pm^2}{2} \frac{\partial}{\partial x_2} \left[(2 + \eta_\pm) \frac{\partial^2 w^\pm}{\partial x_1^2} + \frac{\partial^2 w^\pm}{\partial x_2^2} \right] \right\} = 0, \\ q_1^\pm &:= G_\pm l_\pm^2 \left\{ \frac{\partial^2 w^\pm}{\partial x_2^2} - \eta_\pm \frac{\partial^2 w^\pm}{\partial x_1^2} \right\} = 0. \end{aligned} \quad (12)$$

Assuming also that no tangential line load Q is applied along the crack edge, we enforce that

$$\mu_{22}^+ - \mu_{22}^- = -G_+ l_+^2 (1 + \eta_+) \frac{\partial^2 w^+}{\partial x_1 \partial x_2} \Big|_{(x_1, x_2) = (0^-, 0^+)} + G_- l_-^2 (1 + \eta_-) \frac{\partial^2 w^-}{\partial x_1 \partial x_2} \Big|_{(x_1, x_2) = (0^-, 0^-)} = 0. \quad (13)$$

The formulation is completed by the transmission conditions for ideal interface, which imply continuity of the displacements, rotations, reduced stress and couple-stress components for $x_2 = 0$ and $x_1 > 0$:

$$\begin{aligned} \llbracket w \rrbracket &= 0, \quad \left[\frac{\partial w}{\partial x_2} \right] = 0, \\ \left[G \left\{ \frac{\partial w}{\partial x_2} - \frac{l^2}{2} \frac{\partial}{\partial x_2} \left[(2 + \eta) \frac{\partial^2 w}{\partial x_1^2} + \frac{\partial^2 w}{\partial x_2^2} \right] \right\} \right] &= 0, \quad \left[Gl^2 \left\{ \frac{\partial^2 w}{\partial x_2^2} - \eta \frac{\partial^2 w}{\partial x_1^2} \right\} \right] = 0, \end{aligned} \quad (14)$$

where the notation $\llbracket f \rrbracket$ stands for the jump of the function f across the interface: $\llbracket f \rrbracket = f^+ - f^-$.

2.1 Asymptotic analysis and singularity of stresses

Assuming a polar reference system centered at the crack tip, we search for the main asymptotic term of the solution as $r \rightarrow 0$ in the standard form as follows

$$w^\pm(r, \theta) = r^\lambda F_\pm(\theta, \lambda). \quad (15)$$

We are interested in finding the leading term of the asymptotic solution corresponding to finite elastic energy. This requires that $\lambda \geq 3/2$ (see Radi, 2008). It is noted that the values $\lambda = 0$ and $\lambda = 1$ are also admissible, as long as the respective terms in (15) correspond to a rigid body motion (constant displacement) and a uniform deformation (linear displacement), respectively. Moreover, the expression (15) can be used to find more terms in the asymptotic solution in the form $\sum_i r^{\lambda_i} F_\pm(\theta, \lambda_i)$, provided that $|\lambda_i - \lambda_j| < 2, \forall i \neq j$. If more terms are required with exponents differing by 2 or more than 2, then a two-terms asymptotic procedure should be used instead, as explained in Sec. 3.

Keeping into account only the leading term as $r \rightarrow 0$, the governing equation (11) yields the following ODE for the unknown functions F_\pm

$$F_\pm'''' + 2(\lambda^2 - 2\lambda + 2)F_\pm'' + \lambda^2(\lambda - 2)^2 F_\pm = 0. \quad (16)$$

We first investigate the simplest cases $\lambda = 0$ and $\lambda = 1$, for which eq. (16) admits the solutions

$$F_\pm(\theta, 0) = B_1^\pm + B_2^\pm \theta + B_3^\pm \sin 2\theta + B_4^\pm \cos 2\theta, \quad (17)$$

$$F_\pm(\theta, 1) = (B_1^\pm + B_2^\pm \theta) \sin \theta + (B_3^\pm + B_4^\pm \theta) \cos \theta, \quad (18)$$

respectively. Taking into account all boundary and transmission conditions, one can conclude that for $\lambda = 0$ and $\lambda = 1$, eqs. (17) and (18) take, as expected, the forms

$$F_\pm(\theta, 0) = \beta_0, \quad F_\pm(\theta, 1) = \beta_{11} \sin \theta + \beta_{12} \cos \theta, \quad (19)$$

respectively.

One can also use the representation (15) to find the solution for the case $\lambda = 2$, since the term corresponding to $\lambda = 0$ is not involved in the analysis (as it vanishes after differentiation). Thus, for $\lambda = 2$, eq. (16) admits the solution

$$F_\pm(\theta, 2) = B_1^\pm + B_2^\pm \theta + B_3^\pm \sin 2\theta + B_4^\pm \cos 2\theta, \quad (20)$$

which, taking into account all boundary and transmission conditions, reduces to

$$F_\pm(\theta, 2) = \beta_{21} (\cos^2 \theta + \eta_\pm \sin^2 \theta) + \beta_{22} \sin 2\theta. \quad (21)$$

For all other cases, eq. (16) admits the following solution:

$$F_\pm(\theta) = B_1^\pm \sin(\lambda\theta) + B_2^\pm \cos(\lambda\theta) + B_3^\pm \sin[(\lambda - 2)\theta] + B_4^\pm \cos[(\lambda - 2)\theta]. \quad (22)$$

By imposing the boundary and transmission conditions, we obtain a 8×8 homogeneous algebraic system, whose characteristic equation is

$$\sin^2(\pi\lambda) [\cos(2\pi\lambda) + \kappa] = 0, \quad (23)$$

where $\kappa = C/D > 0$ for any $\eta_\pm > -1$ and

$$\begin{aligned} C &= G_+^2 l_+^4 (5 - 2\eta_- + \eta_-^2) (3 - \eta_+)^2 (1 + \eta_+)^2 + G_-^2 l_-^4 (5 - 2\eta_+ + \eta_+^2) (3 - \eta_-)^2 (1 + \eta_-)^2 \\ &\quad + 2G_+ l_+^2 G_- l_-^2 (3 + \eta_+ + \eta_- - \eta_+ \eta_-) (3 - \eta_+) (1 + \eta_+) (3 - \eta_-) (1 + \eta_-), \\ D &= (3 - \eta_+) (1 + \eta_+) (3 - \eta_-) (1 + \eta_-) \{ G_+^2 l_+^4 (3 - \eta_+) (1 + \eta_+) + G_-^2 l_-^4 (3 - \eta_-) (1 + \eta_-) \\ &\quad + 2G_+ l_+^2 G_- l_-^2 (5 - \eta_+ - \eta_- + \eta_+ \eta_-) \}. \end{aligned} \quad (24)$$

The first term in eq. (23) leads to the conclusion that $\lambda = 3$ (the cases $\lambda = 0, 1, 2$ have been investigated above), while the second term may exhibit singular behaviour depending on the value of the parameter κ . If $\kappa > 1$, then the solution of eq. (23) is complex and the singularity shows oscillatory behaviour in the vicinity of the crack tip. Otherwise, the solution is real and there are no oscillations. More precisely, since κ is strictly positive, the following three cases may occur:

- (i) $0 < \kappa < 1$: the first admissible value of the exponent is in the interval $3/2 < \lambda < 7/4$ (simple root).
- (ii) $\kappa = 1$: the first admissible value of the exponent is $\lambda = 3/2$ (double root).
- (iii) $\kappa > 1$: the first admissible value of the exponent is $\lambda = 3/2 \pm i\gamma$ (simple root), where

$$\gamma = \frac{1}{2\pi} \log(\kappa + \sqrt{\kappa^2 - 1}). \quad (25)$$

In the case of a homogeneous material, $G_+ = G_-$, $l_+ = l_-$, $\eta_+ = \eta_-$, the ratio κ is equal to 1 and thus the first admissible value for the exponent is $3/2$ (this case has been analysed in Radi, 2008). Some other special cases are investigated in the next section.

2.2 Some particular and special cases

To decrease number of parameters, let us first consider the case where $\eta_+ = \eta_- = \eta$. Then the ratio κ reduces to

$$\kappa = \frac{(G_+^2 l_+^4 + G_-^2 l_-^4)(5 - 2\eta + \eta^2) + 2G_+ l_+^2 G_- l_-^2 (3 - \eta)(1 + \eta)}{(G_+^2 l_+^4 + G_-^2 l_-^4)(3 - \eta)(1 + \eta) + 2G_+ l_+^2 G_- l_-^2 (5 - 2\eta + \eta^2)} = \frac{(a^2 + b^2)c + 2ab}{a^2 + b^2 + 2abc}, \quad (26)$$

where we use the notations $a = G_+ l_+^2$, $b = G_- l_-^2$ and

$$c(\eta) = \frac{5 - 2\eta + \eta^2}{(3 - \eta)(1 + \eta)}. \quad (27)$$

Since $c \geq 1$ for any admissible value of η ($-1 < \eta \leq 1$), it is easy to show that, for dissimilar materials, κ is always greater than 1 and equal to 1 if and only if $c = 1$ (or equivalently $\eta = 1$), see Fig. 2.

In the limiting case $\eta = 1$ the asymptotic solution in the vicinity of the crack tip is given by

$$\begin{aligned} w^\pm(r, \theta) = & \beta_0 + r(\beta_1 \sin \theta + \beta_2 \cos \theta) + r^{3/2} \frac{l_\pm^2}{G_\pm} \left\{ \beta_3 \left(3 \sin \frac{\theta}{2} - \sin \frac{3\theta}{2} \right) \right. \\ & \left. + \beta_4 \left(\cos \frac{\theta}{2} - \cos \frac{3\theta}{2} \right) \right\} + r^2 (\beta_5 + \beta_6 \sin 2\theta) + O(r^{5/2}), \quad r \rightarrow 0, \end{aligned} \quad (28)$$

where the constants β_i are amplitude factors depending on far-field loading and specimen geometry. It is noted that logarithmic terms are excluded, since geometric and algebraic multiplicities of the double root coincide (Rössle and Sändig, 1996).

Correspondingly, the asymptotics of symmetric stress, couple-stress and skew-symmetric stress as

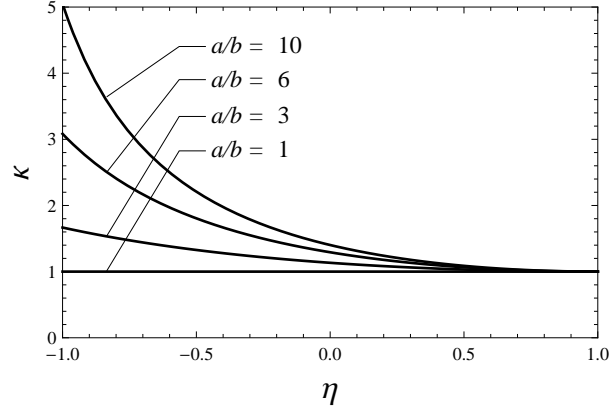


Figure 2: Plot of the ratio κ given by (26) as a function of η for $a/b = 1, 3, 6, 10$.

$r \rightarrow 0$ are

$$\begin{aligned}
\sigma_{13}^{\pm} &= \beta_2 G_{\pm} - 2r^{1/2} l_{\mp}^2 \sin^2 \frac{\theta}{2} \left(3\beta_3 \sin \frac{\theta}{2} + \beta_4 \cos \frac{\theta}{2} \right) + 2r G_{\pm} (\beta_5 \cos \theta + \beta_6 \sin \theta) + O(r^{3/2}), \\
\sigma_{23}^{\pm} &= \beta_1 G_{\pm} + r^{1/2} l_{\mp}^2 \sin \frac{\theta}{2} (3\beta_3 \sin \theta + \beta_4 (3 + \cos \theta)) + 2r G_{\pm} (\beta_5 \sin \theta + \beta_6 \cos \theta) + O(r^{3/2}), \\
\mu_{11}^{\pm} &= -r^{-1/2} l_{+}^2 l_{-}^2 \sin \frac{\theta}{2} [3\beta_3 (\sin \theta + \sin 2\theta) + \beta_4 (2 + \cos \theta + \cos 2\theta)] + 4\beta_6 G_{\pm} l_{\pm}^2 + O(r^{1/2}), \\
\mu_{21}^{\pm} &= \mu_{12}^{\pm} = r^{-1/2} l_{+}^2 l_{-}^2 \left\{ \beta_3 \cos \frac{\theta}{2} (\sin 2\theta - \sin \theta) + \beta_4 \cos \frac{\theta}{2} (2 - \cos \theta + \cos 2\theta) \right\} + O(r^{1/2}), \\
\tau_{13}^{\pm} &= \frac{1}{2} r^{-3/2} l_{+}^2 l_{-}^2 (3\beta_3 \sin \frac{3\theta}{2} + \beta_4 \cos \frac{3\theta}{2}) + O(r^{-1/2}), \\
\tau_{23}^{\pm} &= -\frac{1}{2} r^{-3/2} l_{+}^2 l_{-}^2 (3\beta_3 \cos \frac{3\theta}{2} - \beta_4 \sin \frac{3\theta}{2}) + O(r^{-1/2}).
\end{aligned} \tag{29}$$

Applying now the condition (13), we obtain

$$\mu_{22}^{+}(\theta = \pi) - \mu_{22}^{-}(\theta = -\pi) = \frac{4\beta_4 l_{+}^2 l_{-}^2}{\sqrt{r}} + 4\beta_6 (G_{-} l_{-}^2 - G_{+} l_{+}^2) + O(r^{1/2}), \quad r \rightarrow 0. \tag{30}$$

The limit, as $r \rightarrow 0$, of (30) should equal the tangential line load Q applied to the crack edge. It then appears that β_4 is always zero and β_6 does not vanish only if Q is different from zero. It is also noted that the constant β_3 plays the role of stress intensity factor.

The asymptotics for the crack opening, $\llbracket w \rrbracket = w^{+}(\theta = \pi) - w^{-}(\theta = -\pi)$, and for the skew-symmetric stress ahead of the crack tip, $\tau_{23}^{\pm}(\theta = 0)$, as $r \rightarrow 0$, are given by

$$\llbracket w \rrbracket = 4\beta_3 \frac{G_{+} l_{+}^2 + G_{-} l_{-}^2}{G_{+} G_{-}} r^{3/2} + O(r^{5/2}), \quad \tau_{23}^{\pm}(\theta = 0) = -\frac{3}{2} \beta_3 l_{+}^2 l_{-}^2 r^{-3/2} + O(r^{-1/2}). \tag{31}$$

Therefore, in the vicinity of the crack tip, the skew-symmetric stress at $\theta = 0$ displays a sign opposite to that of the crack opening, in contrast to the classical result of LEFM. A similar effect has been found by Radi (2008) in the case of a crack in an homogeneous CS material.

In the opposite case ($\eta_+ = \eta_- = \eta < 1$), the solution always exhibits oscillatory behaviour near the crack tip. Moreover, this behaviour is quite different from that we encounter in the case of classical materials. In the classic case, the region near the crack tip where the oscillatory behaviour appears is very small, while in the considered case this zone can be quite pronounced or its size can even tend to infinity if $\eta \rightarrow -1$. Taking into account that the asymptotic analysis given here is valid only in a small neighbourhood of the crack tip where the micropolar theory controls the behaviour of the solution, such situation has limited physical meaning.

Let us now assume that the parameters η_+ and η_- are different and one of them, say η_- , tends to the limiting value $\eta_- \rightarrow -1$, while the other is separated from -1 , so that $\eta_+ > -1 + \epsilon$, where ϵ is a small positive parameter. In this case, one can easily check that $\kappa \rightarrow \infty$ for any fixed value of η_+ . This again corresponds to the case where the exponent is a complex number with the imaginary part becoming infinite, $\gamma \rightarrow \infty$, and therefore it has no physical relevance.

It is noted that the case $\eta_- = -1$, $\eta_+ \neq -1$ cannot be recovered from the limiting case discussed above, and thus it will be discussed separately in Sec. 3.3.

Another case of interest is when one of the multipliers involved in the parameter κ , say $G_- l_-^2$, diminishes, $G_- l_-^2 \rightarrow 0$, then

$$\kappa \rightarrow \frac{5 - 2\eta_- + \eta_-^2}{(3 - \eta_-)(1 + \eta_-)} = c(\eta_-) \geq 1. \quad (32)$$

Once again, this solution has physical relevance if and only if $\eta_- = 1$. The assumption $G_- l_- \rightarrow 0$ takes place if one assumes that $l_- \rightarrow 0$, or, in other words, when the material in the lower half-plane reduces to a classical elastic material. This suggests considering the problem of a crack at the interface between a micropolar material (occupying the upper half-plane) and a classical one (occupying the lower half-plane). However, it is not possible to recover from (28) the solution for a classical elastic material, due to the singular perturbation character of the equation (11) as $l_{\pm} \rightarrow 0$. For this reason, the problem of a crack lying at the interface between couple-stress elastic and classical elastic materials is addressed separately in the next section.

2.3 Energy release rate

In this section, the energy release rate is evaluated for the asymptotic representation (28), valid in the case $\eta_+ = \eta_- = 1$, by means of the J -integral argument. The conservation law for couple-stress elasticity (see Lubarda and Markenscoff, 2000) implies that

$$J = \int_{\Gamma} \left(W n_1 - \mathbf{t}^T \mathbf{n} \cdot \frac{\partial \mathbf{u}}{\partial x_1} - \boldsymbol{\mu}^T \mathbf{n} \cdot \frac{\partial \boldsymbol{\varphi}}{\partial x_1} \right) ds = 0, \quad (33)$$

for every closed contour Γ , provided that there is no singularity within Γ . In (33), \mathbf{n} is an outward unit normal on Γ and W denotes the strain-energy density

$$W = G \boldsymbol{\epsilon} \cdot \boldsymbol{\epsilon} + G l^2 (\boldsymbol{\chi} \cdot \boldsymbol{\chi} + \eta \boldsymbol{\chi} \cdot \boldsymbol{\chi}^T). \quad (34)$$

We define $\Gamma^{\pm} = \Gamma_1^{\pm} \cup \Gamma_2^{\pm} \cup \Gamma_{cr}^{\pm} \cup \Gamma_{in}^{\pm}$ (see Fig. 3), so that

$$\sum_{\pm} (J_2^{\pm} \mp J_{cr}^{\pm} - J_1^{\pm} \pm J_{in}^{\pm}) = 0, \quad (35)$$

with evident meaning of the symbols. Then we evaluate each term according to the representation (28), thus obtaining

$$J_1 = J_1^+ + J_1^- = -\frac{2\beta_2\beta_4 l_+^2 l_-^2}{\sqrt{R_1}} + P + O(R_1^{1/2}), \quad (36)$$

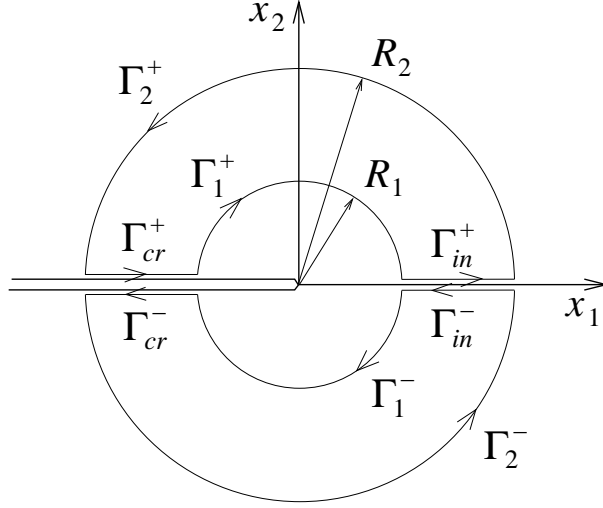


Figure 3: Path of integration for the evaluation of the energy release rate.

$$J_2 = J_2^+ + J_2^- = -\frac{2\beta_2\beta_4 l_+^2 l_-^2}{\sqrt{R_2}} + P + O(R_2^{1/2}), \quad (37)$$

$$J_{cr}^\pm = \pm \frac{\beta_2\beta_4 l_+^2 l_-^2}{\sqrt{R_1}} \mp \frac{\beta_2\beta_4 l_+^2 l_-^2}{\sqrt{R_2}} + O(R_2^{1/2}), \quad (38)$$

$$J_{in}^\pm = -\frac{3\beta_2\beta_3 l_+^2 l_-^2}{\sqrt{R_1}} + \frac{3\beta_2\beta_3 l_+^2 l_-^2}{\sqrt{R_2}} + O(R_2^{1/2}), \quad (39)$$

in which

$$P = \sum_{\pm} \frac{l_{\pm}^2 l_{\mp}^4}{2G_{\pm}} (9\pi\beta_3^2 + \pi\beta_4^2 \pm 12\beta_3\beta_4). \quad (40)$$

Note that the integrals along the interface cancel out from (35), whereas the integrals along the crack faces give

$$J_{cr}^- - J_{cr}^+ = F(R_2) - F(R_1), \quad (41)$$

where

$$F(R) = \frac{2\beta_2\beta_4 l_+^2 l_-^2}{\sqrt{R}} + O(R^{1/2}). \quad (42)$$

It is possible now to introduce a path-independent parameter as follows:

$$J_* = \lim_{R_2 \rightarrow 0} (J_2 + F(R_2)) = \lim_{R_1 \rightarrow 0} (J_1 + F(R_1)) = P. \quad (43)$$

In consideration of the condition (13), β_4 vanishes and the path-independent parameter J_* gives the energy release rate (derived through direct energy balance considerations by Atkinson and Leppington, 1977 and Eshelby, 1980)

$$J_* = \frac{9}{2}\pi l_+^2 l_-^2 \left(\frac{l_-^2}{G_+} + \frac{l_+^2}{G_-} \right) \beta_3^2. \quad (44)$$

In the case of homogeneous body ($G_+ = G_- = G$, $l_+ = l_- = l$), our formula coincides with earlier results by Radi (2008):

$$J_* = \frac{9\pi l^6}{G} \beta_3^2. \quad (45)$$

It is noted here that particular attention should be paid when using the J -integral in CS materials. The contribution of the integrals along the crack faces is not zero, since the force tractions $\mathbf{t}^T \mathbf{n}$ and couple tractions $\boldsymbol{\mu}^T \mathbf{n}$ are not vanishing as in the classical case.

3 Crack at the interface between couple-stress elastic and classical elastic materials

In this section we consider the problem of a crack lying at the interface between a micropolar material (occupying the upper half-plane) and a classical elastic one (occupying the lower half-plane). Then the governing equations are

$$\Delta w^+ - \frac{l^2}{2} \Delta^2 w^+ = 0, \quad \Delta w^- = 0. \quad (46)$$

The traction-free boundary conditions along the crack faces are:

$$p_3^+ = 0 \quad \text{and} \quad q_1^+ = 0 \quad \text{for} \quad \theta = \pi, \quad \sigma_{23}^- = 0 \quad \text{for} \quad \theta = -\pi. \quad (47)$$

Along the ideal interface the continuity of displacement and force tractions needs to be enforced, so that we have the following transmission conditions:

$$w^+ = w^-, \quad p_3^+ = \sigma_{23}^- \quad \text{for} \quad \theta = 0. \quad (48)$$

However, since the orders of the two governing equations are different, an additional transmission condition is needed. This additional condition can be chosen in two different ways. At the boundary of the micropolar material one can prescribe the value of the reduced couple traction q_1^+ , or, alternatively, the value of the rotation φ_1^+ (note that $\varphi_2^+ = \varphi_2^-$ follows immediately from (48)₁). We analyse these two cases separately in the next subsections.

3.1 ‘Couple’ transmission conditions

The additional transmission condition in this case takes the form

$$q_1^+ = 0 \quad \text{for} \quad \theta = 0. \quad (49)$$

Bearing in mind that, in this case, we need to match the solutions of governing equations having different orders, we use here a two-terms asymptotic analysis, so that a solution is searched for in the form

$$w^+(r, \theta) = r^\lambda F_1(\theta) + r^{\lambda+2} F_2(\theta) + O(r^{\lambda+4}), \quad r \rightarrow 0, \quad (50)$$

$$w^-(r, \theta) = r^\lambda H_1(\theta) + r^{\lambda+2} H_2(\theta) + O(r^{\lambda+4}), \quad r \rightarrow 0. \quad (51)$$

Substituting (50) in (46)₁ and collecting like powers of r , we obtain

$$\Delta^2(r^\lambda F_1) = 0, \quad \Delta^2(r^{\lambda+2} F_2) = \frac{2}{l^2} \Delta(r^\lambda F_1). \quad (52)$$

For $\lambda \neq 0, 1, 2$, the system (52) admits the solution

$$\begin{aligned} F_1 &= B_1^{(1)} \sin(\lambda\theta) + B_2^{(1)} \cos(\lambda\theta) + B_3^{(1)} \sin[(\lambda - 2)\theta] + B_4^{(1)} \cos[(\lambda - 2)\theta], \\ F_2 &= B_1^{(2)} \sin[(\lambda + 2)\theta] + B_2^{(2)} \cos[(\lambda + 2)\theta] + B_3^{(2)} \sin(\lambda\theta) + B_4^{(2)} \cos(\lambda\theta) \\ &+ \frac{B_3^{(1)}}{4\lambda l^2} \sin[(\lambda - 2)\theta] + \frac{B_4^{(1)}}{4\lambda l^2} \cos[(\lambda - 2)\theta], \end{aligned} \quad (53)$$

Substituting (51) in (46)₂ and collecting like powers of r , we obtain

$$\Delta(r^\lambda H_1) = 0, \quad \Delta(r^{\lambda+2} H_2) = 0. \quad (54)$$

For $\lambda \neq 0, 1, 2$, the system (54) admits the solution

$$H_1 = A_1^{(1)} \sin \lambda\theta + A_2^{(1)} \cos \lambda\theta, \quad H_2 = A_1^{(2)} \sin[(\lambda + 2)\theta] + A_2^{(2)} \cos[(\lambda + 2)\theta]. \quad (55)$$

Substituting the two-terms asymptotics (50), with $F_{1,2}$ and $H_{1,2}$ given by (53) and (55) respectively, into the boundary and transmission conditions, we obtain a 12×12 homogeneous algebraic system, whose characteristic equation is

$$(1 + \eta) \cos^2(\pi\lambda) \sin^4(\pi\lambda) = 0, \quad (56)$$

so that the exponent λ admits the values $\lambda = k/2$, where $k = 1, 3, 5$.

Note that for $\lambda = 1/2$ the first term in (51) for the classical elastic material corresponds to bounded elastic energy, while the first term in (50) for the micropolar material corresponds to infinite elastic energy. However, from the analysis of all boundary and transmission conditions, it is found that $F_1(\theta) \equiv 0$ in this case, so that the energetic requirements are fulfilled.

For the special cases $\lambda = 0, 1, 2$ the analysis is straightforward and the final asymptotic representation of the solution taking into account all terms $\lambda = k/2$, $k = 0, 1, 2, 3$, is given by

$$\begin{aligned} w^-(r, \theta) &= \alpha_0 + r^{1/2} \alpha_1 \sin \frac{\theta}{2} + r \alpha_2 \cos \theta + r^{3/2} \alpha_3 \sin \frac{3\theta}{2} + r^2 \alpha_4 \cos 2\theta + r^{5/2} \alpha_5 \sin \frac{5\theta}{2} + O(r^3), \quad r \rightarrow 0, \\ w^+(r, \theta) &= \alpha_0 + r(\alpha_2 \cos \theta + \beta_1 \sin \theta) + r^2 \left\{ \alpha_4 \left(\frac{1+\eta}{2} + \frac{1-\eta}{2} \cos 2\theta \right) + \beta_2 \sin 2\theta \right\} \\ &- r^{5/2} \alpha_1 \frac{2G_-}{3G_+ l^2 (3-\eta)} \left\{ \frac{3-5\eta}{5(1+\eta)} \sin \frac{5\theta}{2} + \sin \frac{\theta}{2} \right\} + O(r^3), \quad r \rightarrow 0, \end{aligned} \quad (57)$$

The asymptotics of stress in the lower half-plane, occupied by the classic elastic material, as $r \rightarrow 0$ are given by

$$\begin{aligned} \sigma_{13}^- &= -\frac{1}{2} r^{-1/2} \alpha_1 G_- \sin \frac{\theta}{2} + \alpha_2 G_- + \frac{3}{2} r^{1/2} \alpha_3 G_- \sin \frac{\theta}{2} + 2r \alpha_4 G_- \cos \theta + \frac{5}{2} r^{3/2} \alpha_5 G_- \sin \frac{3\theta}{2} + O(r^2), \\ \sigma_{23}^- &= \frac{1}{2} r^{-1/2} \alpha_1 G_- \cos \frac{\theta}{2} + \frac{3}{2} r^{1/2} \alpha_3 G_- \cos \frac{\theta}{2} - 2r \alpha_4 G_- \sin \theta + \frac{5}{2} r^{3/2} \alpha_5 G_- \cos \frac{3\theta}{2} + O(r^2). \end{aligned} \quad (58)$$

The asymptotics of symmetric stress, couple-stress and skew-symmetric stress in the upper half-plane, occupied by the micropolar material, as $r \rightarrow 0$ are given by

$$\begin{aligned} \sigma_{13}^+ &= \alpha_2 G_+ + 2r G_+ (\alpha_4 \cos \theta + \beta_2 \sin \theta) - \frac{2}{3} r^{3/2} \alpha_1 G_- \frac{1-3\eta+(5-3\eta)\cos\theta}{l^2(3-\eta)(1+\eta)} \sin \frac{\theta}{2} + O(r^2), \\ \sigma_{23}^+ &= \beta_1 G_+ + 2r G_+ (\alpha_4 \eta \sin \theta + \beta_2 \cos \theta) - \frac{2}{3} r^{3/2} \alpha_1 G_- \frac{1+5\eta+(1-7\eta)\cos\theta}{l^2(3-\eta)(1+\eta)} \cos \frac{\theta}{2} + O(r^2), \end{aligned}$$

$$\begin{aligned}
\mu_{11}^+ &= 2\beta_2 G_+ l^2 (1 + \eta) - r^{1/2} \alpha_1 G_- \frac{1 - 3\eta + (1 + \eta) \cos \theta}{3 - \eta} \cos \frac{\theta}{2} + O(r), \\
\mu_{21}^+ &= -r^{1/2} \alpha_1 G_- \frac{(1 + \eta) \sin \theta}{3 - \eta} \cos \frac{\theta}{2} + O(r), \\
\mu_{12}^+ &= -2\alpha_4 G_+ l^2 (1 - \eta^2) + r^{1/2} \alpha_1 G_- \frac{3 - 5\eta - (1 + \eta) \cos \theta}{3 - \eta} \sin \frac{\theta}{2} + O(r), \\
\tau_{13}^+ &= -r^{-1/2} \frac{\alpha_1 G_-}{3 - \eta} \sin \frac{\theta}{2} + O(1), \\
\tau_{23}^+ &= r^{-1/2} \frac{\alpha_1 G_-}{3 - \eta} \cos \frac{\theta}{2} + O(1).
\end{aligned} \tag{59}$$

The condition (13) becomes now $\mu_{22}^+(r=0, \theta=\pi) = 0$, which requires β_2 to vanish, except for the case where a tangential line load is applied along the crack edge.

It is now possible to analyse the jump of the rotation component φ_1 across the interface and it is found that there is a mismatch between the micropolar material and the elastic one given by

$$\llbracket \varphi_1 \rrbracket = -\frac{1}{4} \alpha_1 r^{-1/2} + \frac{1}{2} \beta_1 - \frac{3}{4} \alpha_3 r^{1/2} + \beta_2 r + O(r^{3/2}), \quad r \rightarrow 0. \tag{60}$$

It is concluded that in the classical elastic material the solution shows a square-root singularity, as in the classic case. Moreover, in the micropolar material, the symmetric stress and the couple-stress are bounded, and only the skew-symmetric stress shows a square-root singularity.

The energy release rate, computed in the same manner as in Sec. 2.3, is given by

$$J_* = \frac{\pi}{8} G_- \alpha_1^2, \tag{61}$$

which shows that the constant α_1 plays the role of stress intensity factor.

3.2 ‘Rotation’ transmission conditions

The problem is defined by the equations (46) with the boundary and transmission conditions (47) and (48). The additional transmission condition used here is the continuity of the rotation vector, namely

$$\varphi_1^+ = \varphi_1^- \quad \text{for } \theta = 0. \tag{62}$$

We search for a solution again in the form (50) and (51). For $\lambda \neq 0, 1, 2$, the characteristic equation now takes the form

$$(1 + \eta)^2 \sin^2(\pi\lambda) [1 + \eta - (\eta - 3) \cos 2\pi\lambda]^2 = 0, \tag{63}$$

so that the exponent λ admits real values, namely integer positive numbers and

$$\lambda = \pm \frac{1}{2\pi} \arccos \frac{\eta + 1}{\eta - 3} + k, \tag{64}$$

where k is a non negative integer.

In the particular case $\eta = 1$, the complete asymptotics of the solution up to the fourth order is given by

$$\begin{aligned}
w^-(r, \theta) &= \alpha_0 + r\alpha_1 \cos \theta + r^2\alpha_2 \cos 2\theta + r^3\alpha_3 \cos 3\theta + r^4\alpha_4 \cos 4\theta + O(r^5), \quad r \rightarrow 0, \\
w^+(r, \theta) &= \alpha_0 + r\alpha_1 \cos \theta + r^2\alpha_2 + r^{5/2}\beta_1 \left(\cos \frac{5\theta}{2} - \cos \frac{\theta}{2} \right) + r^3\alpha_3 \left(\frac{3}{2} \cos \theta - \frac{1}{2} \cos 3\theta \right) \\
&+ r^{7/2}\beta_2 \left(\cos \frac{7\theta}{2} - \cos \frac{3\theta}{2} \right) + r^4 \left\{ \left(\frac{\alpha_2}{24l^2} - \alpha_4 \right) \cos 4\theta + \left(2\alpha_4 - \frac{\alpha_2}{6l^2} \right) \cos 2\theta + \frac{\alpha_2}{8l^2} \right\} + O(r^{9/2}), \quad r \rightarrow 0.
\end{aligned} \tag{65}$$

The asymptotics of stress in the classic elastic material occupying the lower half-plane as $r \rightarrow 0$ become

$$\begin{aligned}\sigma_{13}^- &= \alpha_1 G_- + 2r\alpha_2 G_- \cos \theta + 3r^2\alpha_3 G_- \cos 2\theta + 4r^3\alpha_4 G_- \cos 3\theta + O(r^4), \\ \sigma_{23}^- &= -2r\alpha_2 G_- \sin \theta - 3r^2\alpha_3 G_- \sin 2\theta - 4r^3\alpha_4 G_- \sin 3\theta + O(r^4),\end{aligned}\tag{66}$$

Finally, the asymptotics of symmetric stress, couple-stress and skew-symmetric stress in the micropolar material occupying the upper half-plane as $r \rightarrow 0$ become

$$\begin{aligned}\sigma_{13}^+ &= \alpha_1 G_+ + 2r\alpha_2 G_+ \cos \theta - 3r^{3/2}\beta_1 G_+ \sin \theta \sin \frac{\theta}{2} + 3r^2\alpha_3 G_+ \\ &\quad - 10r^{5/2}\beta_2 G_+ \sin^2 \frac{\theta}{2} \left(2 \cos \frac{\theta}{2} + \cos \frac{3\theta}{2} \right) + 4r^3\alpha_4 G_+ \cos \theta (2 - 2 \cos \theta) + O(r^{7/2}), \\ \sigma_{23}^+ &= 2r\alpha_2 G_+ \sin \theta - \frac{1}{2}r^{3/2}\beta_1 G_+ \left(3 \sin \frac{\theta}{2} + 7 \sin \frac{3\theta}{2} \right) + 3r^2\alpha_3 G_+ \sin 2\theta \\ &\quad + \frac{1}{2}r^{5/2}\beta_2 G_+ \left(5 \sin \frac{\theta}{2} - 9 \sin \frac{5\theta}{2} \right) + \frac{2}{3l^2}r^3 G_+ \sin \theta [\alpha_2 - (\alpha_2 - 18\alpha_4 l^2) \cos 2\theta] + O(r^{7/2}), \\ \mu_{11}^+ &= -\frac{3}{2}r^{1/2}\beta_1 G_+ l^2 \left(5 \sin \frac{\theta}{2} + \sin \frac{3\theta}{2} \right) + 12r\alpha_3 G_+ l^2 \sin \theta - \frac{5}{2}r^{3/2}\beta_2 G_+ l^2 \left(3 \sin \frac{\theta}{2} + 7 \sin \frac{3\theta}{2} \right) \\ &\quad + 24r^2\alpha_4 G_+ l^2 \sin 2\theta + O(r^{5/2}), \\ \mu_{21}^+ &= \mu_{12}^+ = -\frac{3}{2}r^{1/2}\beta_1 G_+ l^2 \left(5 \cos \frac{\theta}{2} - \cos \frac{3\theta}{2} \right) + \frac{5}{2}r^{3/2}\beta_2 G_+ l^2 \left(3 \cos \frac{\theta}{2} - 7 \cos \frac{3\theta}{2} \right) \\ &\quad + 4r^2 G_+ \sin^2 \theta (\alpha_2 - 12\alpha_4 l^2) + O(r^{5/2}), \\ \tau_{13}^+ &= \frac{3}{2}r^{-1/2}\beta_1 G_+ l^2 \cos \frac{\theta}{2} - 6\alpha_3 G_+ l^2 + \frac{15}{2}r^{1/2}\beta_2 G_+ l^2 \cos \frac{\theta}{2} - 24r\alpha_4 G_+ l^2 \cos \theta + O(r^{3/2}), \\ \tau_{23}^+ &= \frac{3}{2}r^{-1/2}\beta_1 G_+ l^2 \sin \frac{\theta}{2} - \frac{15}{2}r^{1/2}\beta_2 G_+ l^2 \sin \frac{\theta}{2} - 4r G_+ (\alpha_2 - 6\alpha_4 l^2) \sin \theta + O(r^{3/2}).\end{aligned}\tag{67}$$

In this case, the reduced couple traction q_1 along the interface has the form:

$$q_1^+(r, \theta = 0) = -6r^{1/2}\beta_1 G_+ l^2 - 10r^{3/2}\beta_2 G_+ l^2 + O(r^{5/2}), \quad r \rightarrow 0.\tag{68}$$

Of course, it is possible to construct the asymptotic solution for arbitrary $|\eta| < 1$. However, the general form for arbitrary η is rather complicated. As an additional example, we provide the result for $\eta = 1/3$ and up to the first four terms ($\lambda = 0, 1/3, 2/3, 1$):

$$\begin{aligned}w^-(r, \theta) &= \alpha_0 + r\alpha_1 \cos \theta + r^2\alpha_2 \cos 2\theta + r^{7/3}\alpha_3 \left(\sin \frac{7\theta}{3} - \frac{1}{\sqrt{3}} \cos \frac{7\theta}{3} \right) \\ &\quad + r^{8/3}\alpha_4 \left(\sin \frac{8\theta}{3} - \frac{1}{\sqrt{3}} \cos \frac{8\theta}{3} \right) + O(r^3), \quad r \rightarrow 0, \\ w^+(r, \theta) &= \alpha_0 + r\alpha_1 \cos \theta + r^2\alpha_2 \left(\frac{2}{3} + \frac{1}{3} \cos 2\theta \right) \\ &\quad + r^{7/3}\alpha_3 \left(\frac{10}{9} \sin \frac{7\theta}{3} - \frac{10}{3\sqrt{3}} \cos \frac{7\theta}{3} - \frac{7}{9} \sin \frac{\theta}{3} + \frac{7}{3\sqrt{3}} \cos \frac{\theta}{3} \right) \\ &\quad + r^{8/3}\alpha_4 \left(\frac{11}{9} \sin \frac{8\theta}{3} + \frac{11}{3\sqrt{3}} \cos \frac{8\theta}{3} - \frac{8}{9} \sin \frac{2\theta}{3} - \frac{8}{3\sqrt{3}} \cos \frac{2\theta}{3} \right) + O(r^3), \quad r \rightarrow 0.\end{aligned}\tag{69}$$

It is found that the behaviour of the displacement and stress fields is similar for any $-1 < \eta \leq 1$. In particular, stresses are always bounded in the classical elastic material, while in the micropolar

material singular behaviour appears only in the skew-symmetric stress (with different level of singularity depending on the value of η). Moreover, the energy release rate is always zero for any $-1 < \eta \leq 1$. This shows that this type of transmission conditions does not allow for the propagation of the crack along the interface, and thus has limited physical meaning.

3.3 The special case $\eta_- = -1$ and $\eta_+ \neq -1$

In the particular case of $\eta_- = -1$ and $\eta_+ \neq -1$, the governing equation (11) and the traction-free crack face conditions (12) for the material in the lower half-plane are satisfied by the classical solution defined by the field equation

$$\Delta w^- = 0, \quad (70)$$

together with the following boundary condition

$$\frac{\partial w^-}{\partial x_2} = 0 \quad \text{for } x_1 < 0, x_2 = 0. \quad (71)$$

Moreover, in this case the couple-stress and skew-symmetric stress fields in the lower half-plane identically vanish, so that the transmission conditions along the interface $x_1 > 0, x_2 = 0$ become

$$w^+ = w^-, \quad p_3^+ = \sigma_{23}^-, \quad (72)$$

together with one of the following additional conditions

$$q_1^+ = 0, \quad \varphi_1^+ = \varphi_1^-, \quad (73)$$

which correspond to the cases investigated in Secs. 3.1 and 3.2, respectively.

4 Discussion and conclusions

In the present work, the effects of strain rotation gradients on a stationary Mode III crack along the interface between dissimilar couple-stress elastic materials have been analytically investigated by performing an asymptotic analysis of the crack tip fields. It is shown that solutions without oscillations appear in the following two cases: when the two materials are the same (homogeneous material) and when the two materials are dissimilar but $\eta_+ = \eta_- = 1$. In the latter case, the solution displays the same $r^{-3/2}$ singularity (appearing in the skew-symmetric stress components) as for the problem of a crack in an homogeneous CS material. In other cases, the solution exhibits oscillatory behaviour in the vicinity of the crack tip, with the overlapping zone becoming increasingly large as the ratio η between the characteristic lengths in one of the materials approaches the value -1 . The energy release rate has been calculated by means of the conservation J -integral. It is shown that contributions of the integrals along the crack faces have to be retained and the additional boundary condition along the crack edge (Koiter, 1964) is essential to guarantee that the generalized J -integral (Lubarda and Markenscoff, 2000) remains bounded. This additional boundary condition has always been omitted in the earlier literature because so far only the symmetrical problem in homogeneous materials was discussed. The boundary condition along the crack edge breaks the symmetry and becomes fundamental for interface problems.

The special problem of a crack along the interface between couple-stress and classical elastic materials has also been addressed. Two types of transmission conditions have been considered: ‘couple’ and ‘rotation’ transmission conditions. In the former case, it is assumed that the couple-stress traction is continuous, and thus vanishes, at the interface. In the latter, it is assumed instead that the rotations are continuous at the interface. It turns out that the solutions are quite different in the two cases and it is not possible to satisfy simultaneously both type of transmission conditions, so that a mismatch is

always present at the interface, resulting either in a non-balanced couple-stress or a discontinuity in the micro-rotations. It is shown also that the special case $\eta_- = -1$ and $\eta_+ \neq -1$ reduces to the problem of a crack at the interface between classical and couple-stress elastic materials.

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